

Erratum

The technical note **Deviation from Darcy's law observed in one-dimensional consolidation**, *Géotechnique*, **53**, No. 6, 601–605, was incorrectly listed as Deviation for Darcy's law observed in one-dimensional consolidation on the contents page and back cover of the issue.

At the top of page 604 the text should have read:

The settlement observed in the test area is shown in Fig. 5.

The captions for figures 4 and 5 have been transposed and should have read as follows:

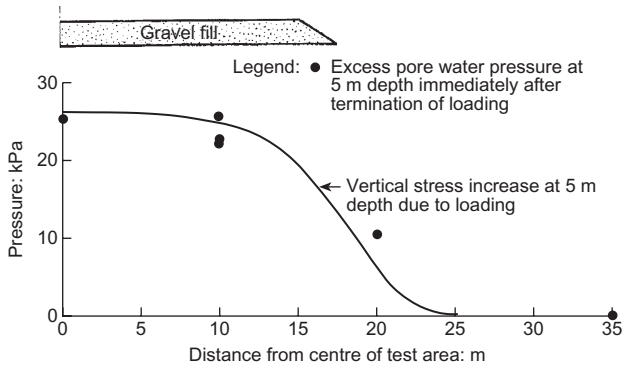


Fig. 4. Consolidation settlement of ground surface and compression of clay layer between 2.5 and 7.5 m depth observed in Test Area IV

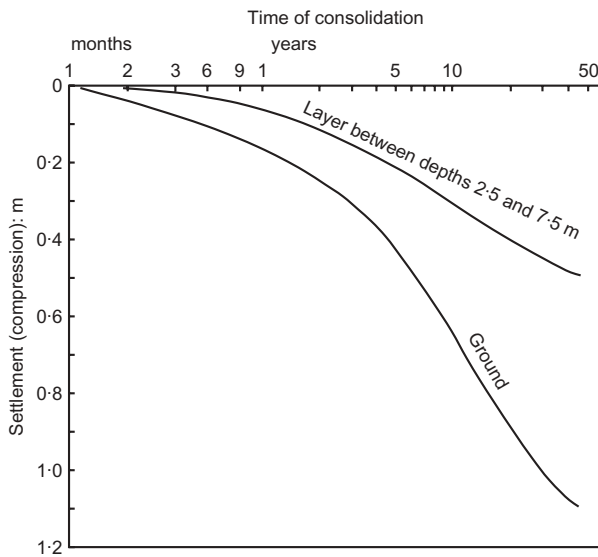


Fig. 5. Observed excess pore pressure distribution in Test Area IV at 5 m depth, immediately after placement of gravel fill

The following errors were printed in the paper **An elasto-plastic model for unsaturated soil incorporating the effects of suction and degree of saturation on mechanical behaviour**, *Géotechnique*, **53**, No. 1, 123–135:

In page 127/line 2 ... should read as *Figures 6 and 7 show for the data sets of Sharma (1998) and Sivakumar (1993) respectively*

Equations (2), (8), (9) and (10) should have read:

$$\sigma''_{hk} = \sigma_{hk} - \delta_{hk}[u_a - S_r(u_a - u_w)] \quad (2)$$

$$\Delta e = -\kappa \ln \frac{p''_o(\xi_2)}{p''_o(0)} \quad (8)$$

$$\Delta e = e(p''_o(\xi_2), \xi_2) - e(p''_o(0), 0) = \frac{e}{e_s}(\xi_2)[N - \lambda \ln p''_o(\xi_2)] - N + \lambda \ln p''_o(0) \quad (9)$$

$$\ln p''_o(\xi_2) = \frac{\lambda - \kappa}{\frac{e}{e_s}(\xi_2)\lambda - \kappa} \ln p''_o(0) + \frac{\left(\frac{e}{e_s}(\xi_2) - 1\right)N}{\frac{e}{e_s}(\xi_2)\lambda - \kappa} \quad (10)$$

NOTATION

a, b	model parameters
e	void ratio
e_s	void ratio in saturated conditions
e_w	water ratio
Δe^e	elastic change of void ratio
Δe^p	plastic change of void ratio
$f(s)$	Fisher function
$\bar{p}$	isotropic net stress
p''	isotropic average skeleton stress
$p''_o(0)$	yield stress in saturated conditions
$p''_o(\xi)$	yield stress in unsaturated conditions
s	suction
u_a	pore air pressure
u_w	pore water pressure
S_r	degree of saturation
κ	elastic swelling index
λ	slope of the saturated normal compression line
N	intercept of the saturated normal compression line at $p'' = 1$ kPa
ξ	bonding variable
σ	total stress
$\bar{\sigma}$	net stress
σ'	Bishop stress
σ''	average skeleton stress
χ	Bishop stress parameter

In the paper, **Effective stress in unsaturated soil: a microstructural analysis** *Géotechnique* **53**, No. 2, 273–277 the following errors were published:

- On the upper left corner of Fig. 1 (p. 274), the label should be $(u_a - u_w)\lambda$
- In the third line after Eq. 2 (p. 274), $u_i = \phi$ should be $u_i = 0$
- In the 6th line after Eq. 2 (p. 274), u_{ij} should be $u_{i,j}$
- In the 6th line after Eq. 2 (p. 274), w_k should be ω_k
- In the second line of Eq. 23, the + sign in the brackets should be – the correct equation is below

$$F_{ij} = S_r \delta_{ij} + \frac{1}{V} \left[\int_{\Gamma} x_i \lambda_j d\Gamma - \sum_{m=1}^{N^p} x_i^{c_m} \left(\int_{S_w^m} n_j dA + \int_{\Gamma^m} \lambda_j d\Gamma \right) \right] \\ = S_r \delta_{ij} - \frac{1}{V} \sum_{m=1}^{N^p} x_i^{c_m} \int_{S_w^m} n_j dA + \frac{1}{V} \left[\int_{\Gamma} x_i \lambda_j d\Gamma - \sum_{m=1}^{N^p} x_i^{c_m} \int_{\Gamma^m} \lambda_j d\Gamma \right] \\ \triangleq S_r \delta_{ij} + \xi'_{ij} + \xi''_{ij}$$

The following errors were published in **Proposal for a new plasticity chart**, *Géotechnique*, **53**, No. 4, 397–406:

On page 397, 2nd column, line 20 up: the reference should be to (D 2487). On page 398, 1st column, line 2 the reference should be to (BS 1377). In Fig. 3: The label for the diamond symbol should be W_p .

Corrected versions of the papers can be viewed by subscribers on www.geotechnique-ice.com.